

COMSOL CONFERENCE 2016 MUNICH

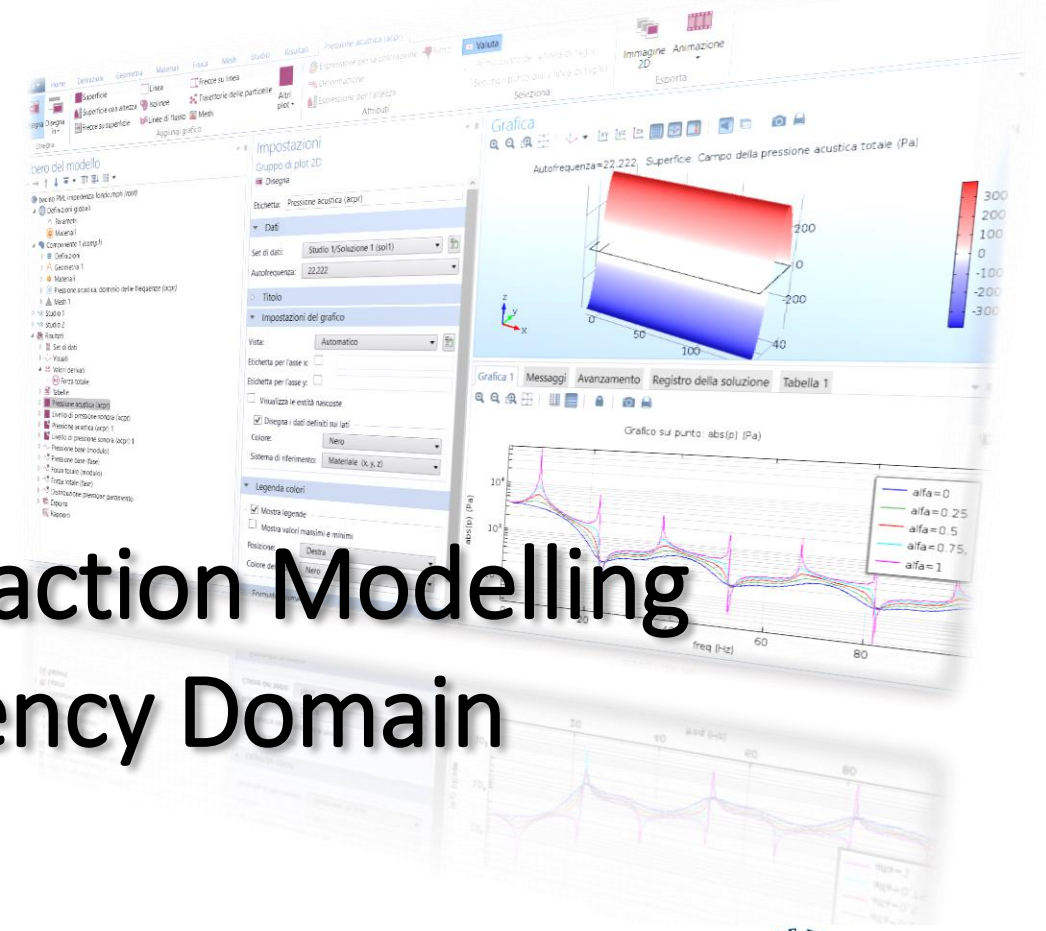
Acoustic Fluid-Structure Interaction Modelling of Gravity Dams in the Frequency Domain

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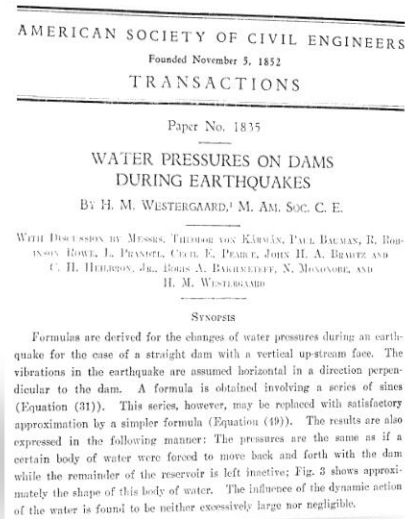
COMSOL

Adoption of the acoustic formulation:

Previous works:

H. M. Westergaard (1933) - A. K. Chopra (1967)

«... Since the involved motions are small, the relatively simple equations may be used, that apply to sound in liquids. ... »



Author's assumptions:

- Null global flow
- Rigid dam
- Infinite-length reservoir
- Small displacements of the fluid particles
- Bidimensional problem (2D)

$$\nabla^2 p = \frac{1}{c^2} \cdot \frac{\partial^2 p}{\partial t^2}$$

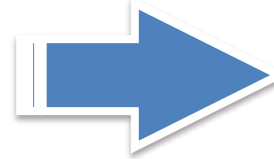
Westergaard added mass method:

Fourier series solution for particle displacement:

$$\xi = -\frac{\alpha g T^2}{\pi^2} \cos\left(\frac{2\pi t}{T}\right) \sum_{1,3,5 \dots}^n \frac{1}{n} e^{-q_n} \sin\left(\frac{n\pi y}{2h}\right)$$

$$\eta = \frac{\alpha g T^2}{\pi^2} \cos\left(\frac{2\pi t}{T}\right) \sum_{1,3,5 \dots}^n \frac{1}{n c_n} e^{-q_n} \cos\left(\frac{n\pi y}{2h}\right)$$

$$c_n = \sqrt{1 - \frac{16wh^2}{n^2 g k T^2}}$$

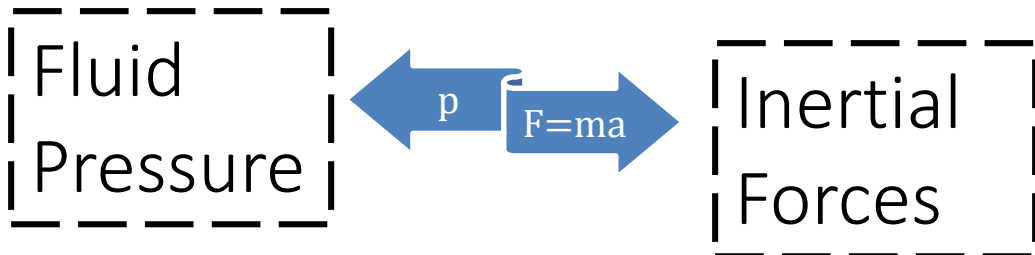
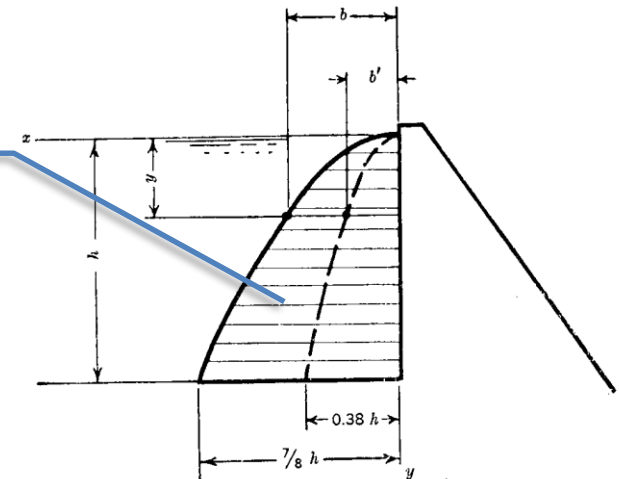


Reservoir period(s):

$$T_n = \frac{4h}{c \cdot n}$$

Added Water Mass:

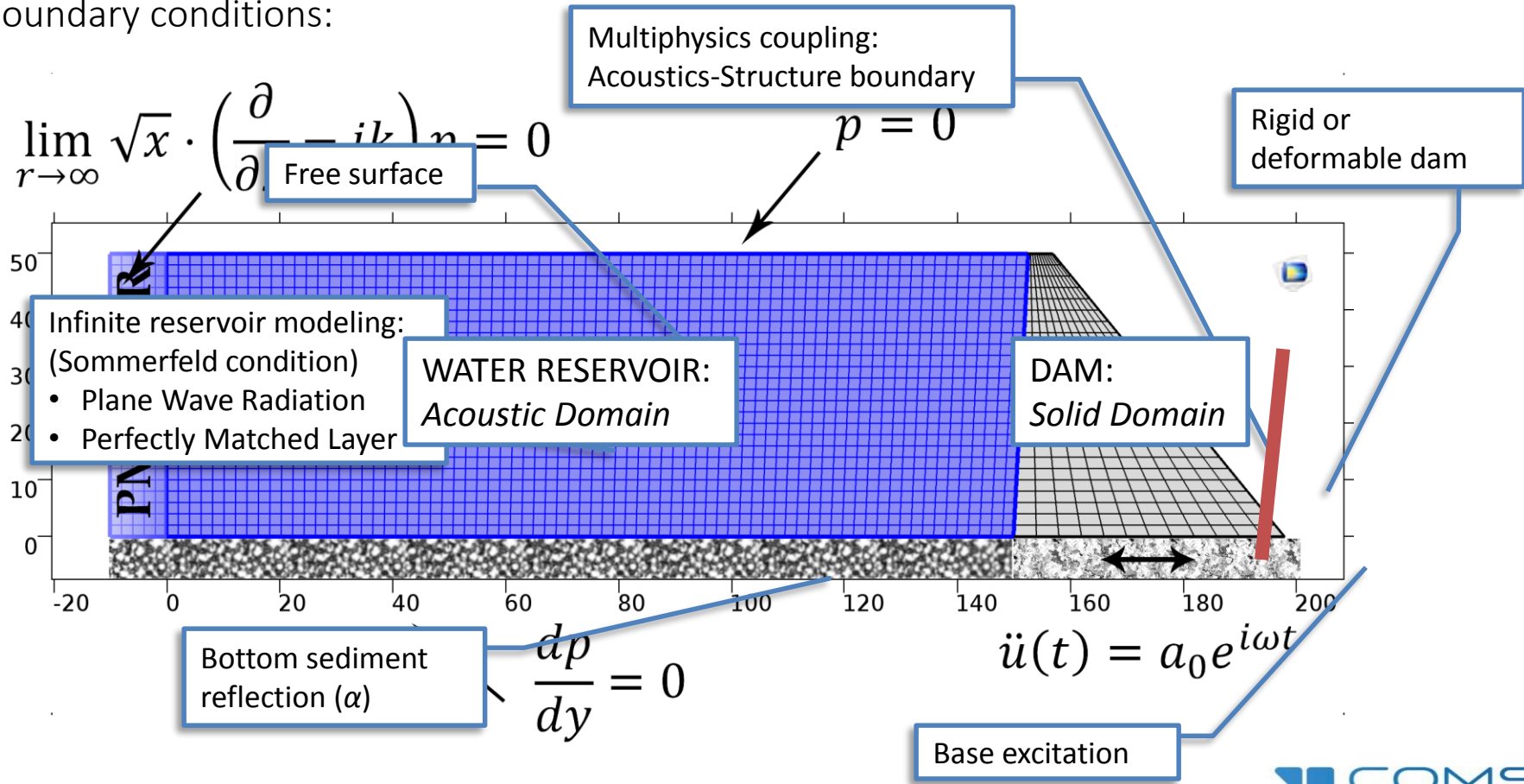
$$b(y) = \frac{7}{8} \sqrt{hy}$$



The COMSOL® model:

- Pressure acoustics interface – frequency domain Structural mechanics

Boundary conditions:



Modeling the Infinte

Two approaches:

- **Plane wave radiation (PWR):** Robin boundary condition, second order

$$-\mathbf{n} \cdot \left(-\frac{1}{\rho_c} (\nabla p_t - \mathbf{q}_d) \right) + i \frac{k}{\rho_c} p + \frac{i}{2k\rho_c} \Delta_T p = Q_i \quad 0$$

No monopole or dipole sources

- **Perfectly matched layer (PML):** Complex coordinate transformation
 - Rational scaling:

$$f_r(\xi) = s\lambda\xi \left(\frac{1}{3p(1-\xi) + 4} - \frac{i}{3p(1-\xi)} \right)$$

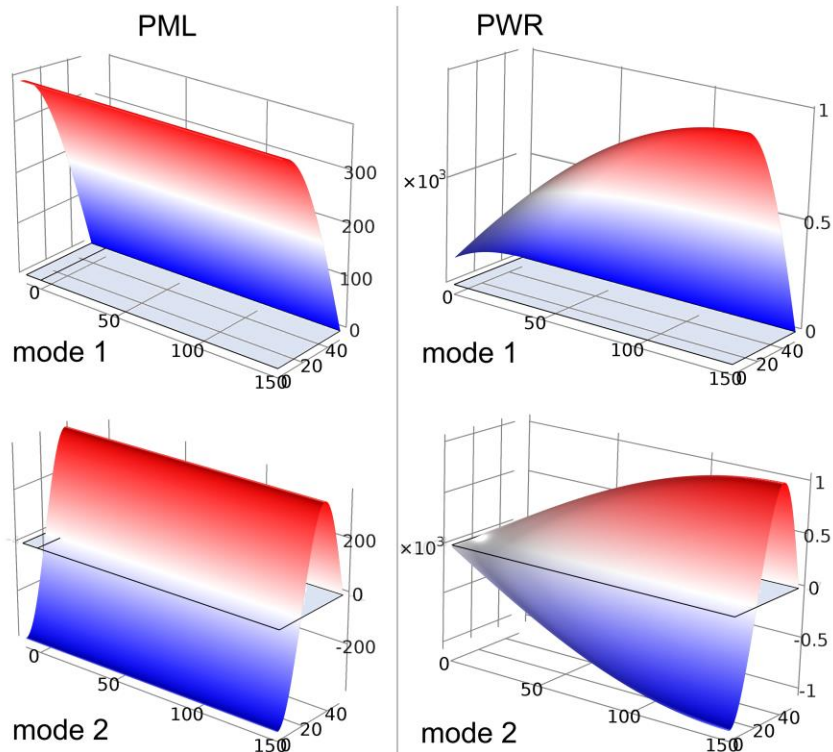
ξ = Dimensionless coordinate, $[0,1]$

s = Scaling parameter, p = curvature parameter

Λ = Typical wavelength parameter

Results: PML vs. PWR - Modal analysis

- Case (a): Rigid dam with perfect bottom reflection ($\alpha=1$)



✘ PWR:
Symmetry
violated

✔ PML:
Symmetry
respected

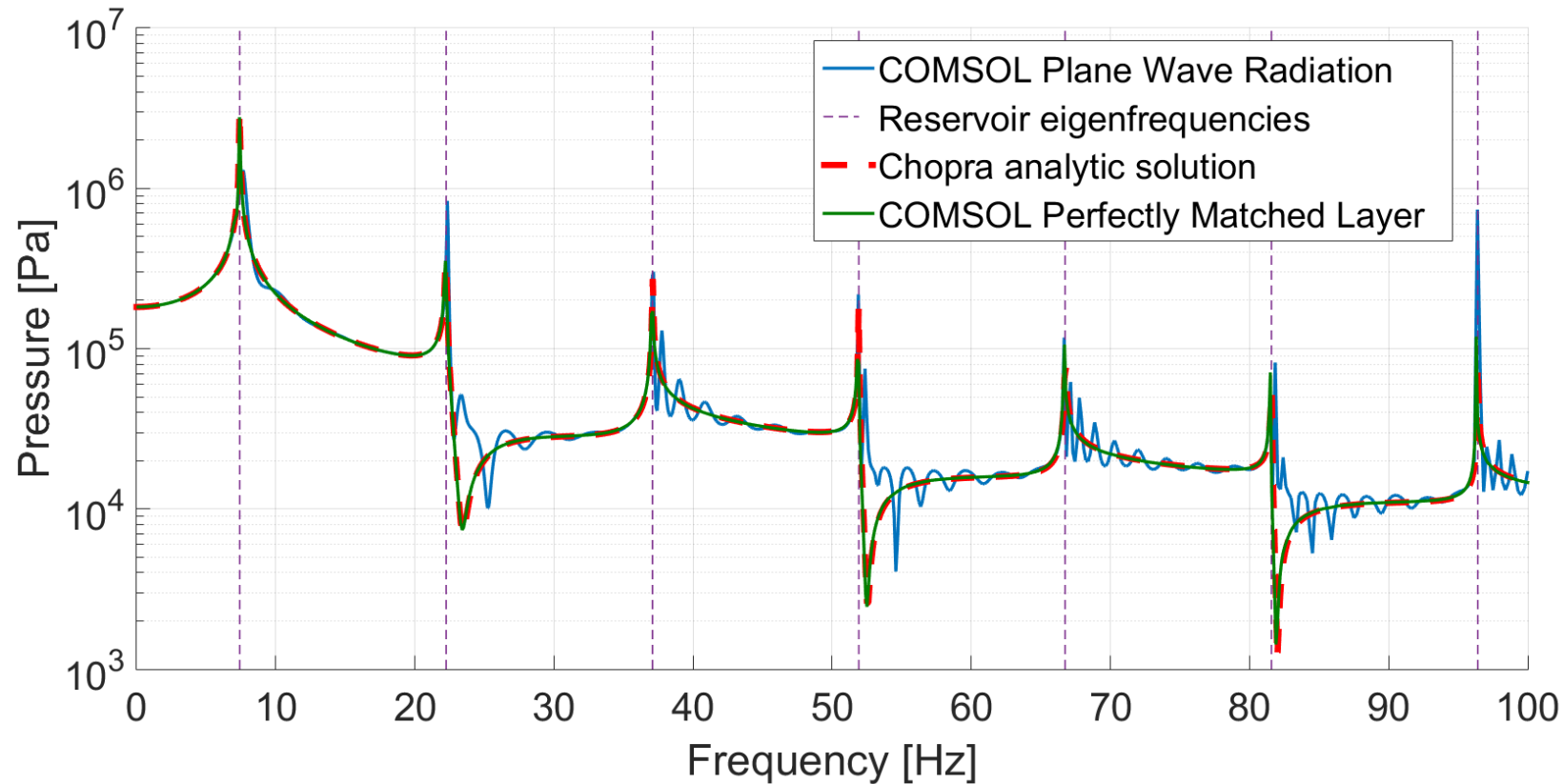
Reservoir depth = 50 m

Eigen mode	Analytic $\left(\frac{nc}{4h}\right)$ [Hz]	PWR [Hz]	PML [Hz]
1	7.407	7.817	7.407
2	22.221	22.386	22.222
3	37.035	37.164	37.036
4	51.849	51.976	51.851
5	66.663	66.720	66.667

Plot: First two eigenmodes, height is proportional to water pressure

Results: PML vs. PWR – Frequency response

- Case (a): Rigid dam with perfect bottom reflection ($\alpha=1$)



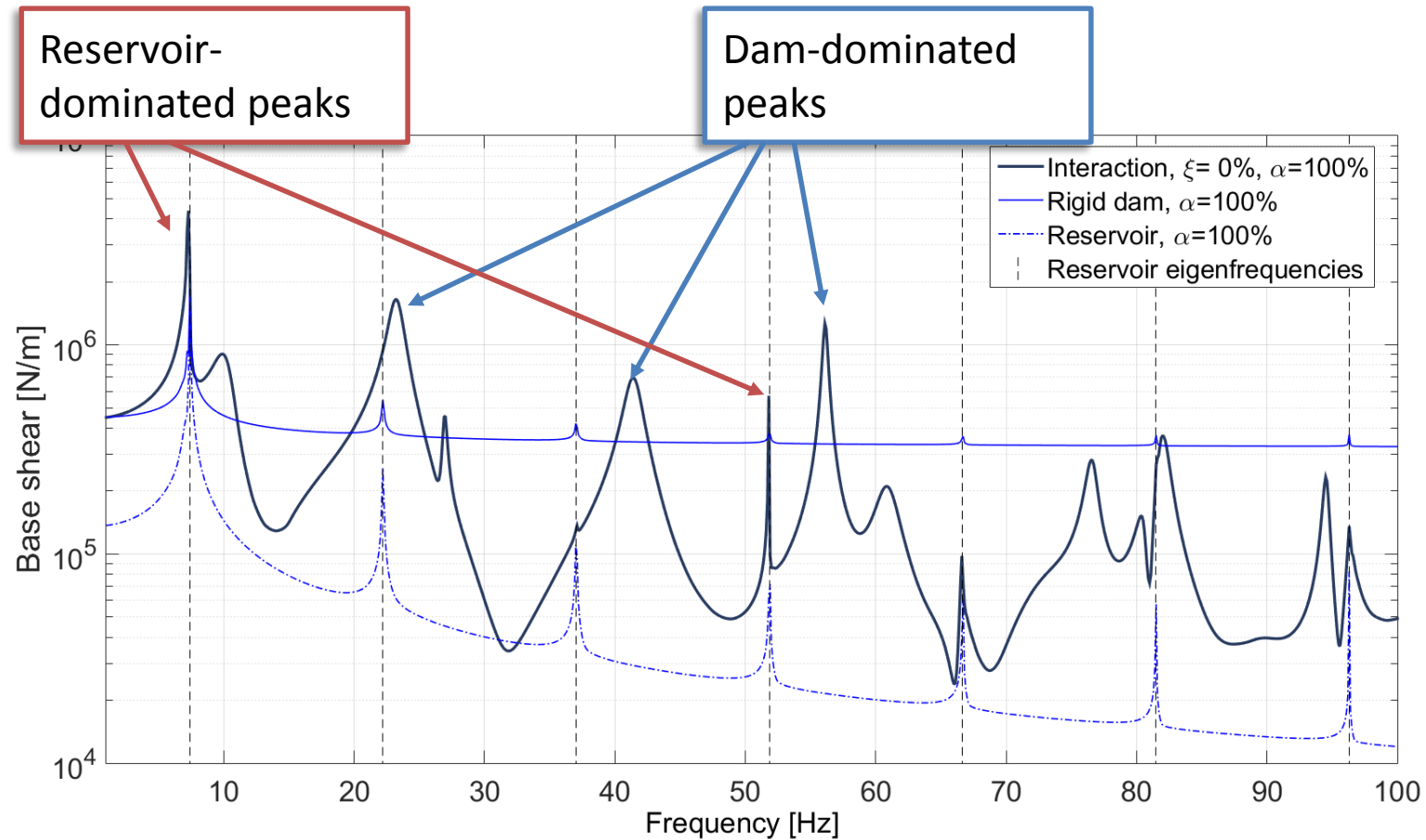
✘ **PWR:**
Introduction of
spurious peaks

✔ **PML:**
Correct
modeling of the
infinite-length
reservoir

Plot: Total hydrodynamic pressure at the base of the dam.

Results: Multiphysics interaction

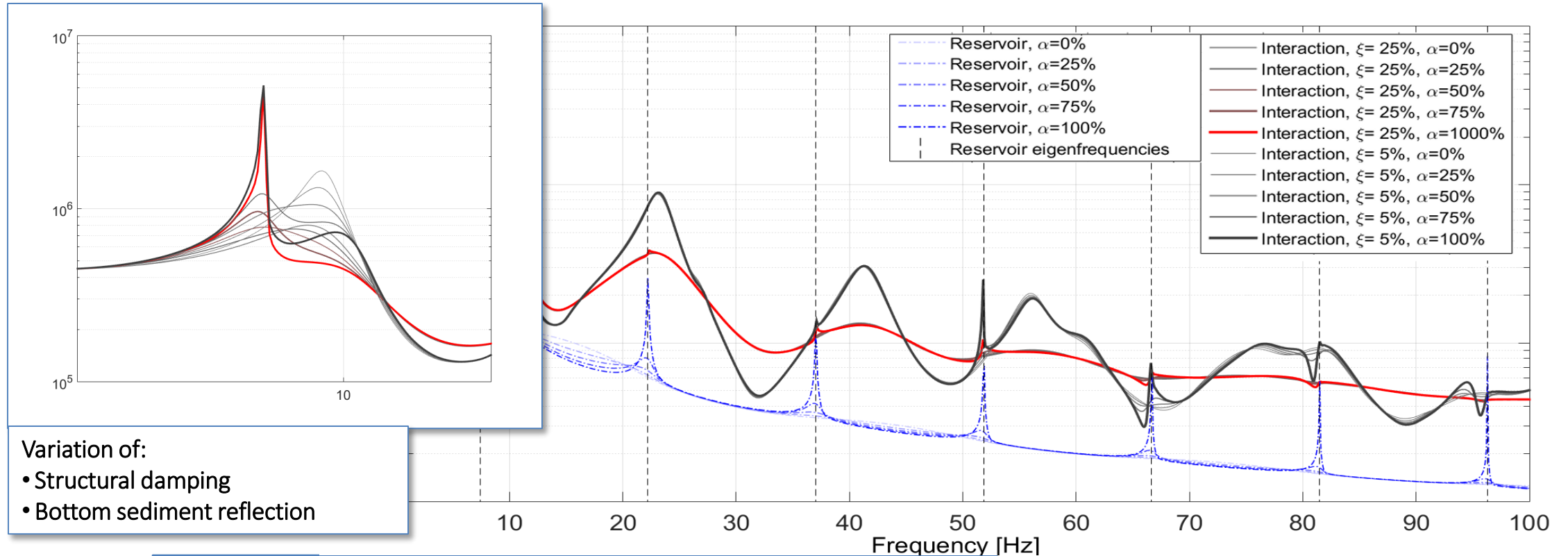
- Case (b): Deformable dam with perfect bottom reflection ($\alpha=1$)



Plot: Horizontal base reaction at the dam foundation.

Results: Multiphysics interaction

- Case (b): Deformable dam with various reflection coefficients (α)



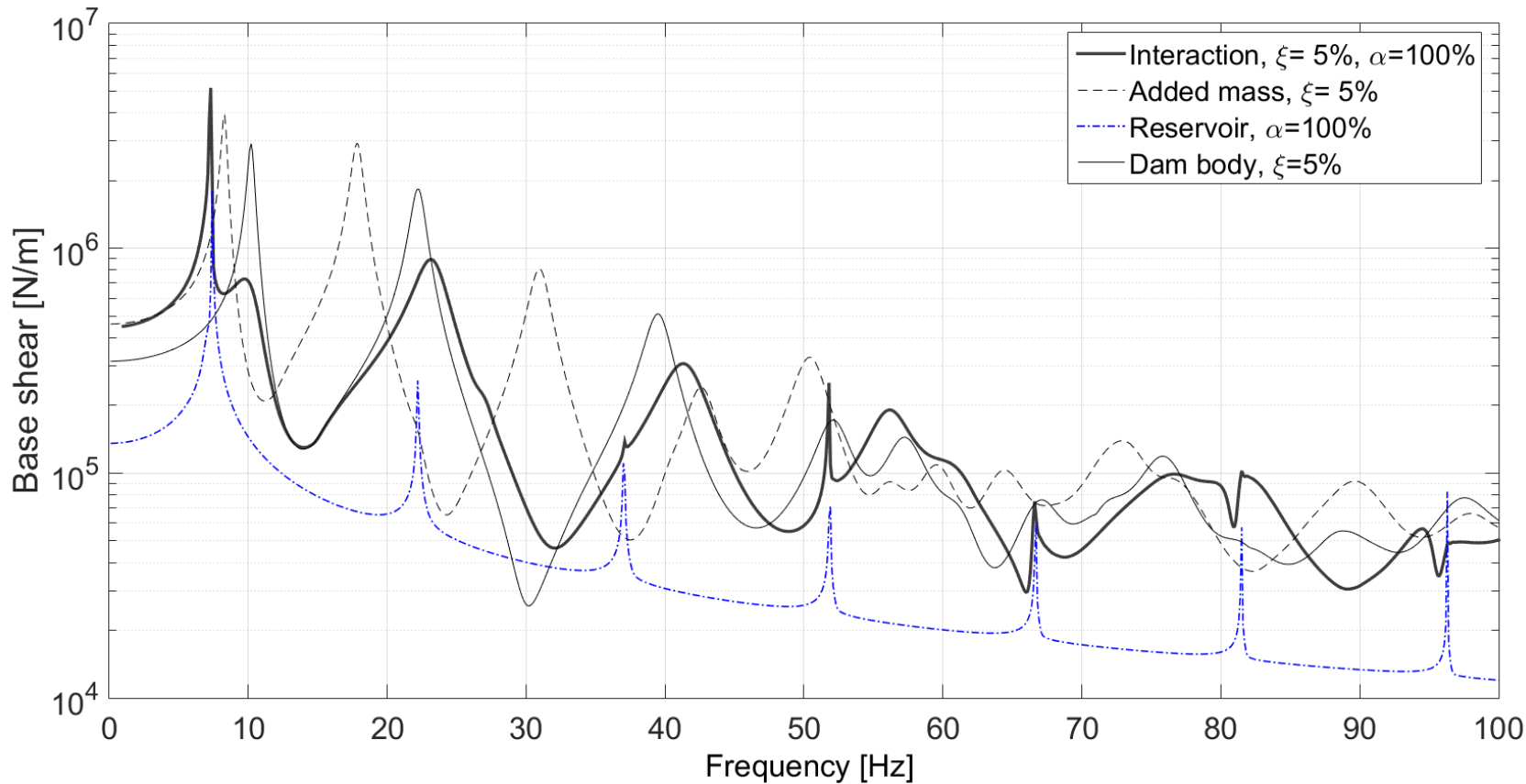
Variation of:

- Structural damping
- Bottom sediment reflection

Plot: Horizontal base reaction at the dam foundation.

Results: Multiphysics interaction

- Case (b): Deformable dam compared to the added mass method



Added mass:

✘ Inaccurate
Identification
of other peaks

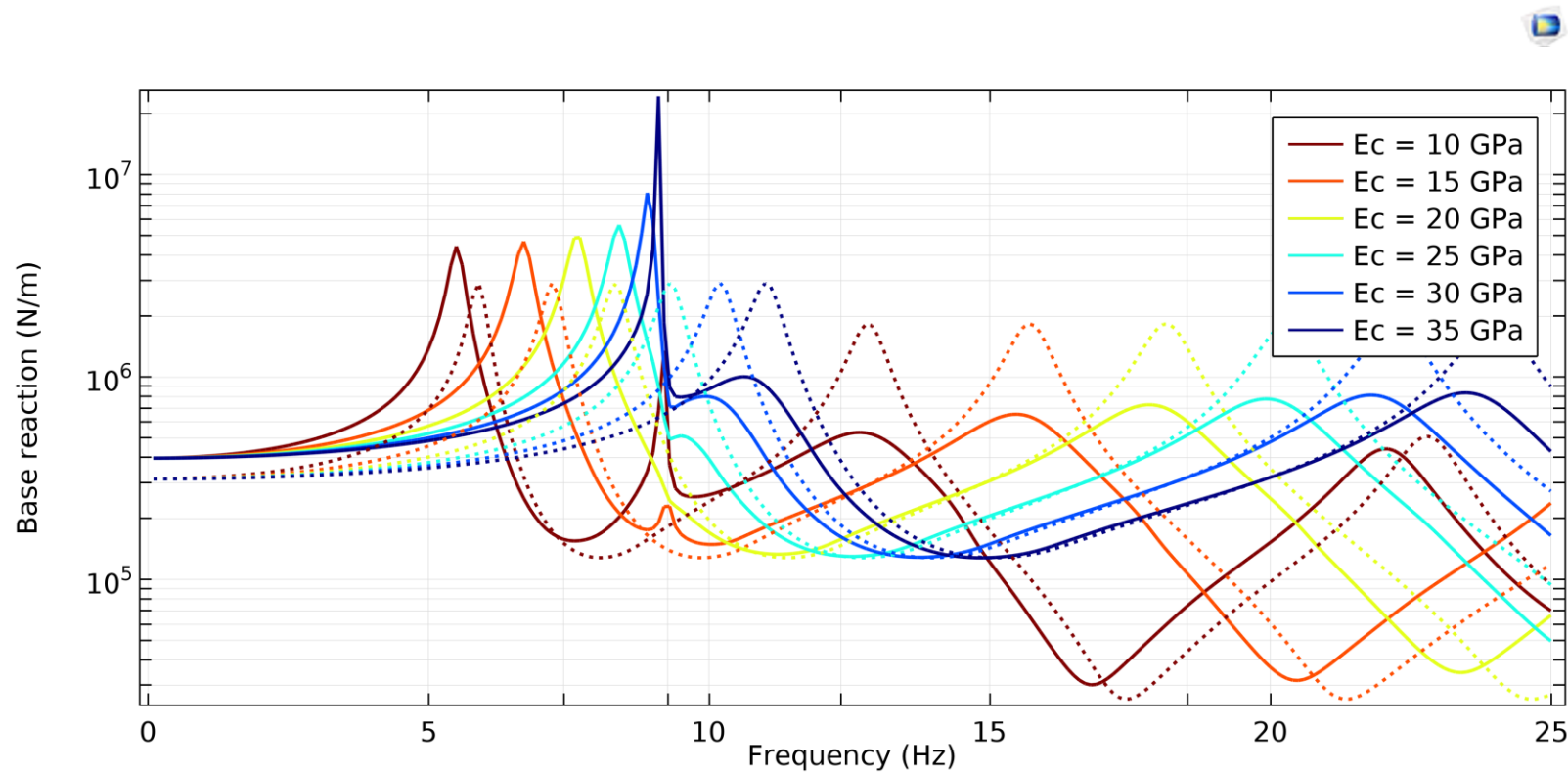
✔ Approximate
Identification of
the first mode

✔ Accurate value
of base shear
For low
frequencies

Plot: Horizontal base reaction at the dam foundation.

Results: Multiphysics interaction

- Case (b): Variation of dam Young's modulus



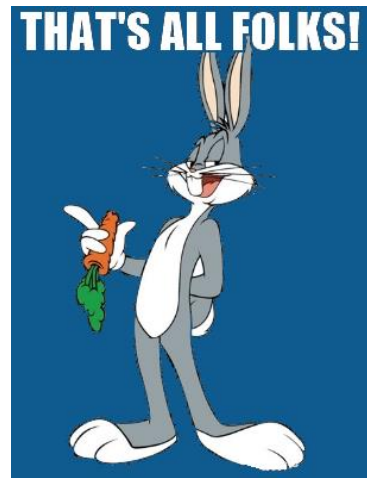
Plot: Horizontal base reaction at the dam foundation.

Added mass:

✘ Constant frequency shift of the peak

Acoustic-structure interaction:

✔ Accurate representation of the nonlinear Frequency shift



Thanks for your attention!