

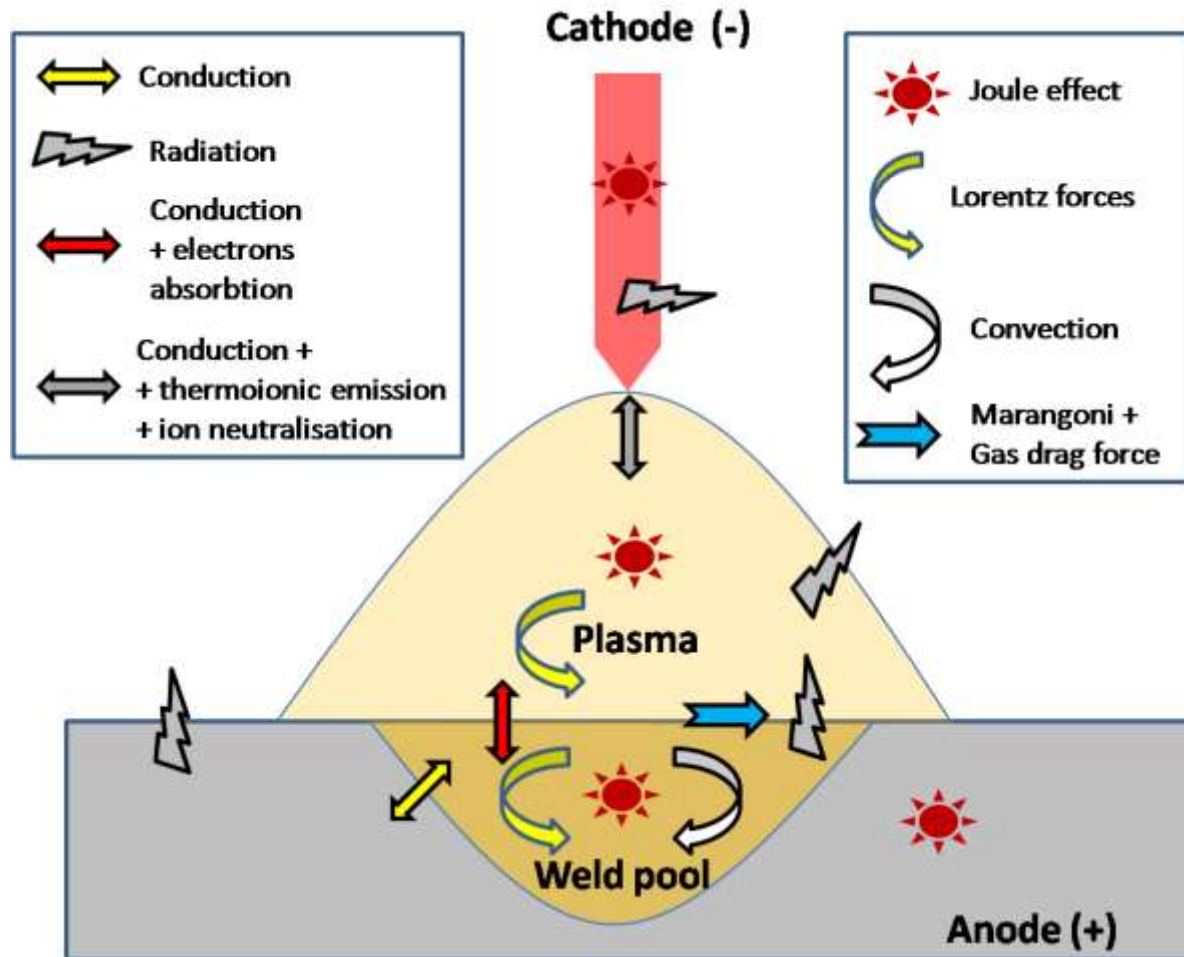
A Transient Unified Model of Arc Weld Pool Couplings during Spot GTA Welding

A. TRAUDIA, and F. Roger

ENSTA-Paristech & AREVA NP, FRANCE

COMSOL Conference, Boston 2010

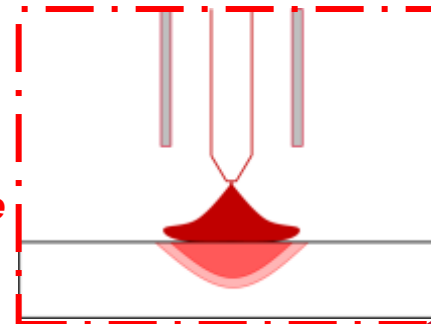
► Gas Tungsten Arc Welding – Tungsten Inert Gas



A highly coupled multiphysics problem

► State of art – Towards a unified formulation

Cathode
+
Plasma
+
Stainless steel anode
(weld pool)

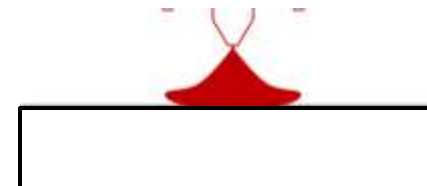


Lowke, Tanaka et al
(1992, 1997, ..., 2010)

Hsu et al (1982, ...)



Gonzalez et al (1993, 1998, 2005, ...)



Plasma
+
Cooled copper anode
(No weld pool)

► Toward a unified model

Mathematical formulation

Inside the cathode, plasma, and anode

$$\nabla \cdot \left(\sigma \nabla V + \sigma \frac{\partial \vec{A}}{\partial t} \right) = 0$$

$$\sigma \frac{\partial \vec{A}}{\partial t} + \nabla \times \left(\frac{1}{\mu_0} \nabla \times \vec{A} \right) + \sigma \nabla V = \vec{0}$$

$$\nabla \cdot \vec{v} = 0$$

$$\rho \left(\frac{\partial \vec{v}}{\partial t} + \vec{v} \cdot \nabla \vec{v} \right) = - \nabla p + \mu \nabla \cdot (\nabla \vec{v} + {}^t \nabla \vec{v})$$

$$+ \vec{j} \times \vec{B} + \rho_0 \vec{g} + w_p \rho_0 \beta (T - T_{ref}) \vec{g}$$

$$\rho C_p^{eq} \left(\frac{\partial T}{\partial t} + \vec{v} \cdot \nabla T \right) = \nabla \cdot (\lambda \nabla T) + \vec{j} \cdot \vec{E}$$

$$+ \frac{5k_B}{2e} \vec{j} \cdot \nabla T - (1 - w_p) \cdot 4\pi \epsilon_N$$

$$P_a - \lambda - \rho g \varphi = -\gamma \frac{r \varphi_{rr} + \varphi_r (1 + \varphi_r^2)}{r (1 + \varphi_r^2)^{\frac{3}{2}}}$$

$$\lambda + \rho g (L + \psi) = -\gamma \frac{r \psi_{rr} + \psi_r (1 + \psi_r^2)}{r (1 + \psi_r^2)^{\frac{3}{2}}}$$

Main boundary conditions

Plasma-cathode interface

$$[-k \nabla T \cdot (-\vec{n})]_{cathode} - [-k \nabla T \cdot (-\vec{n})]_{plasma} = j_i V_i - j_e \phi_c - \epsilon \sigma_B T^4$$

Plasma-anode interface

$$[-k \nabla T \cdot (-\vec{n})]_{anode} - [-k \nabla T \cdot (-\vec{n})]_{plasma} = |\vec{j} \cdot \vec{n}| \phi_a - \epsilon \sigma_B T^4$$

$$\mu \frac{\partial(\vec{v} \cdot \vec{s})}{\partial \vec{n}} = \vec{\tau}_a + f_L \frac{\partial \gamma}{\partial T} \frac{\partial T}{\partial \vec{s}}$$

$$\frac{\partial \gamma}{\partial T} = -A_\gamma - R_s \Gamma_s \ln(1 + Ka_s) - \frac{Ka_s}{1 + Ka_s} \Gamma_s \frac{\Delta H_0}{T}$$

$$K(T) = k_1 \exp\left(-\frac{\Delta H_0}{R_s T}\right)$$

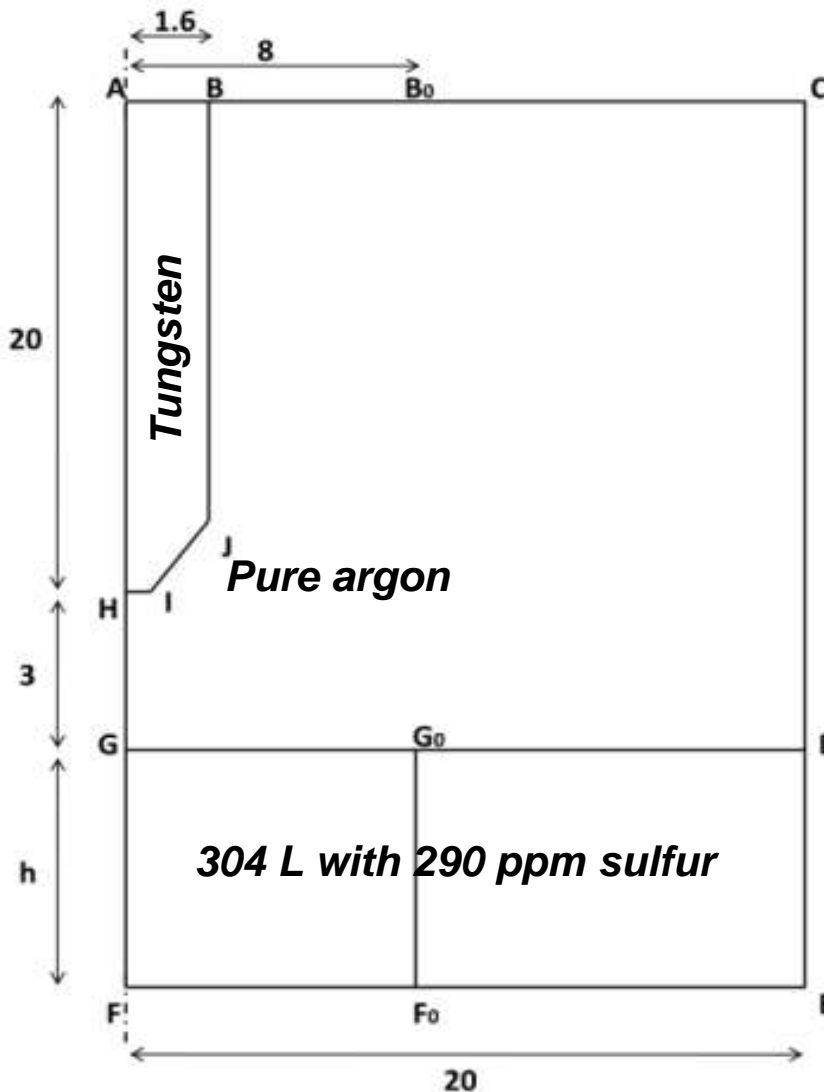
Free surfaces of the weld pool

$$\vec{\tau} = \mu \frac{\partial(\vec{v} \cdot \vec{s})}{\partial \vec{n}} = f_L \frac{\partial \gamma}{\partial T} \frac{\partial T}{\partial \vec{s}}$$

$$\vec{q} \cdot \vec{n} = h(T - T_0)$$

$$\int_0^{rt} 2\pi \varphi(r) r dr = \int_0^{rb} 2\pi \psi(r) r dr$$

Application to pulsed current welding



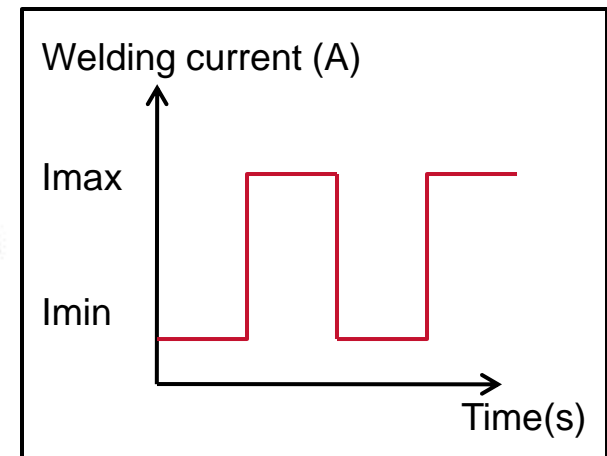
80/160 A

1 Hz

$\alpha 60^\circ$

Arc length 3 mm

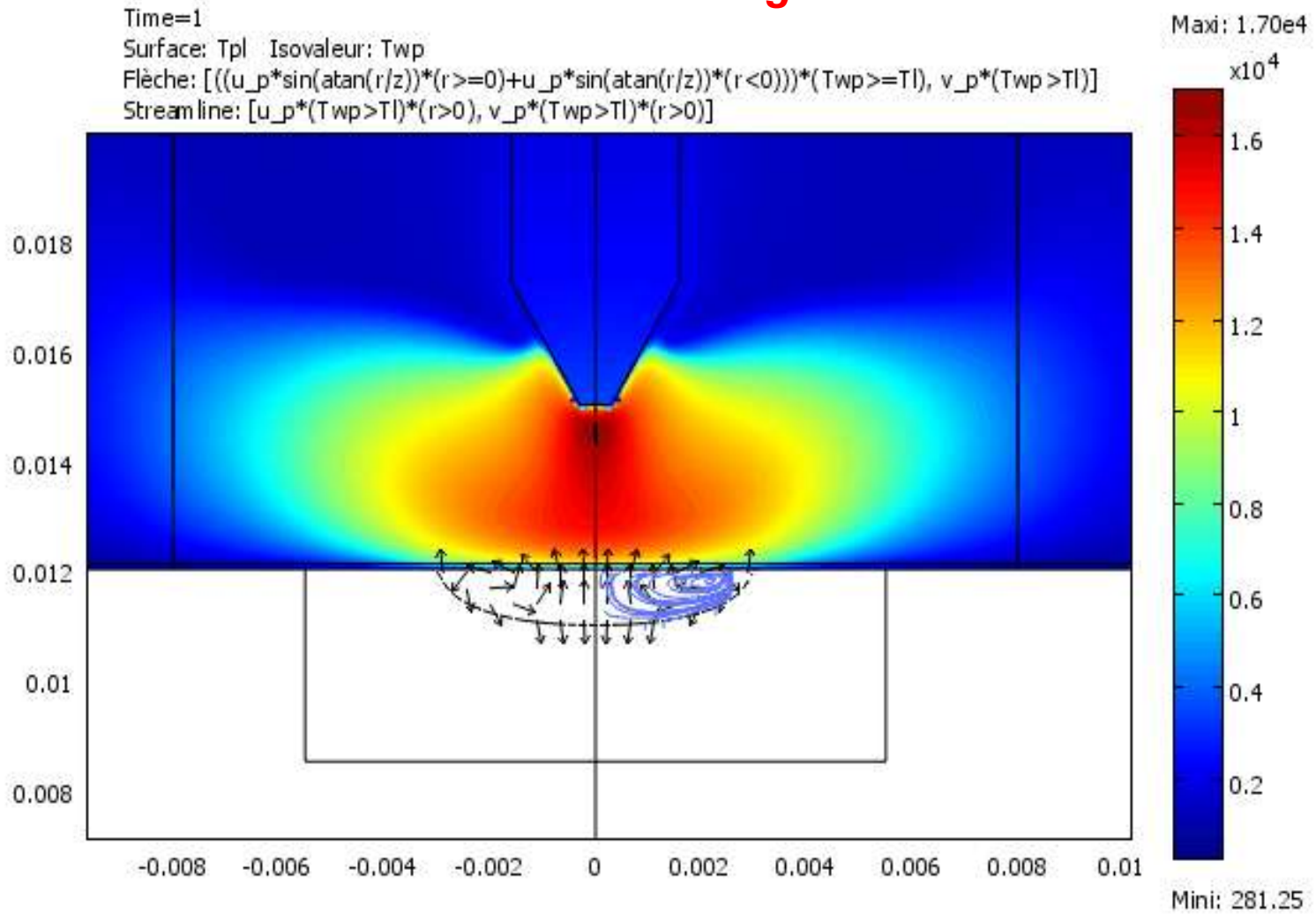
Heating time: 15 s



► Results

Application to pulsed current welding

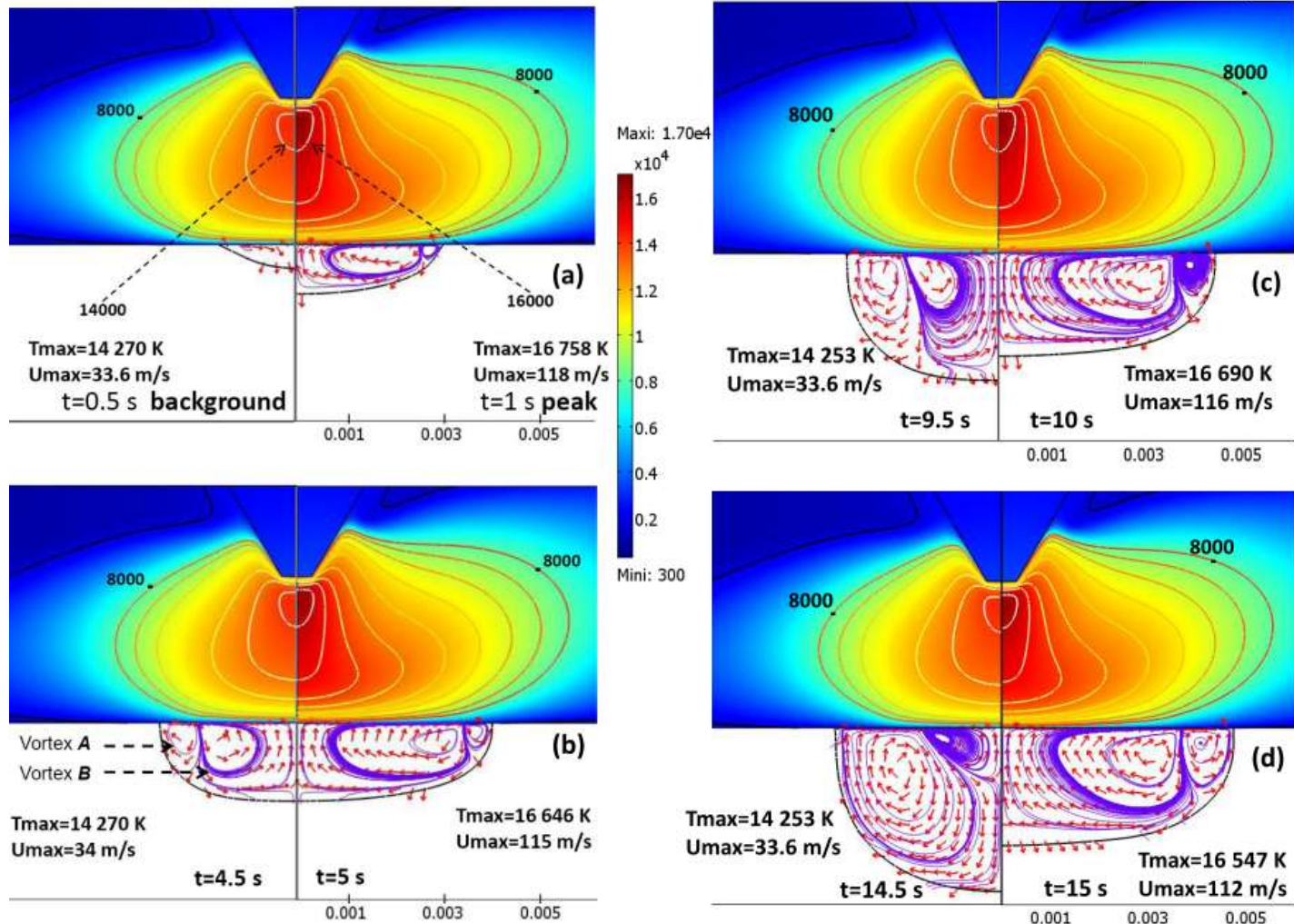
80/160 A- 1 Hz
 α 60°- h 3 mm



► Results

Application to pulsed current welding

80/160 A- 1 Hz
 α 60°- h 3 mm



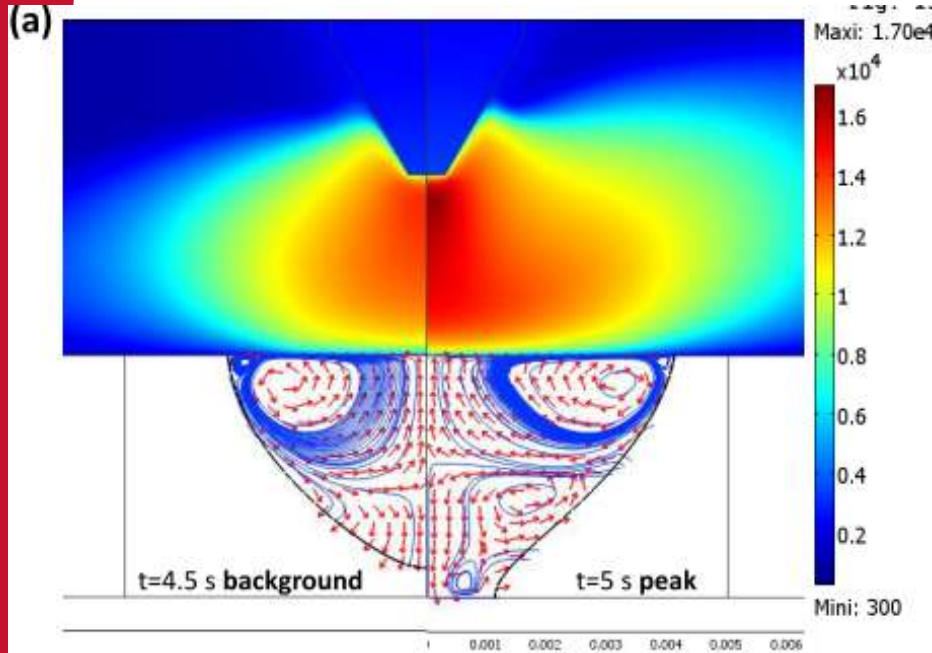
Details about the weld pool evolution in: A. Traidia, F. Roger, E. Guyot. "Optimal parameters for pulsed gas tungsten arc welding in partially and fully penetrated weld pools". *IJTS* 2010.

► Results

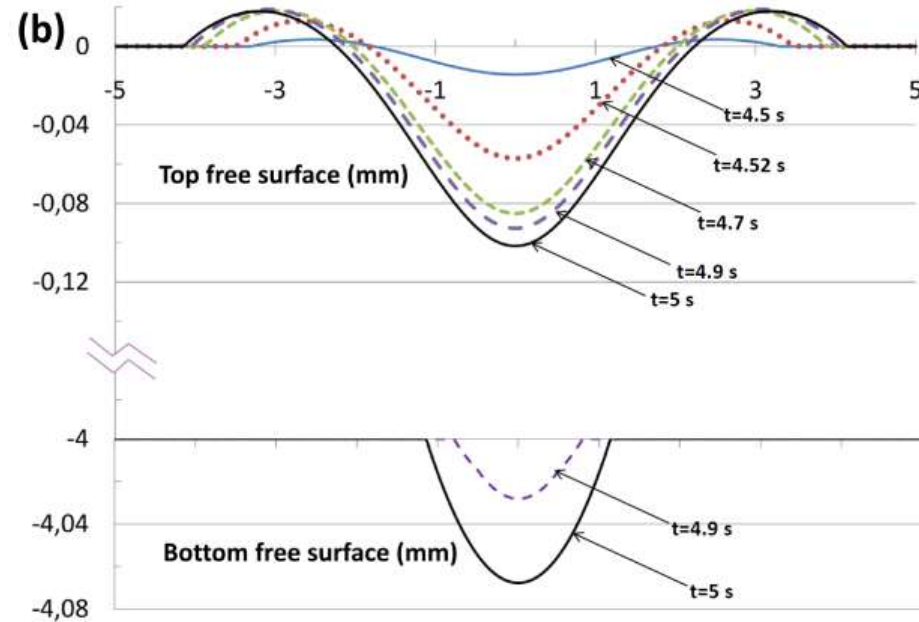
Application to pulsed current welding

80/160 A- 1 Hz
 α 60°- h 3 mm

► *Fully penetrated weld pool*



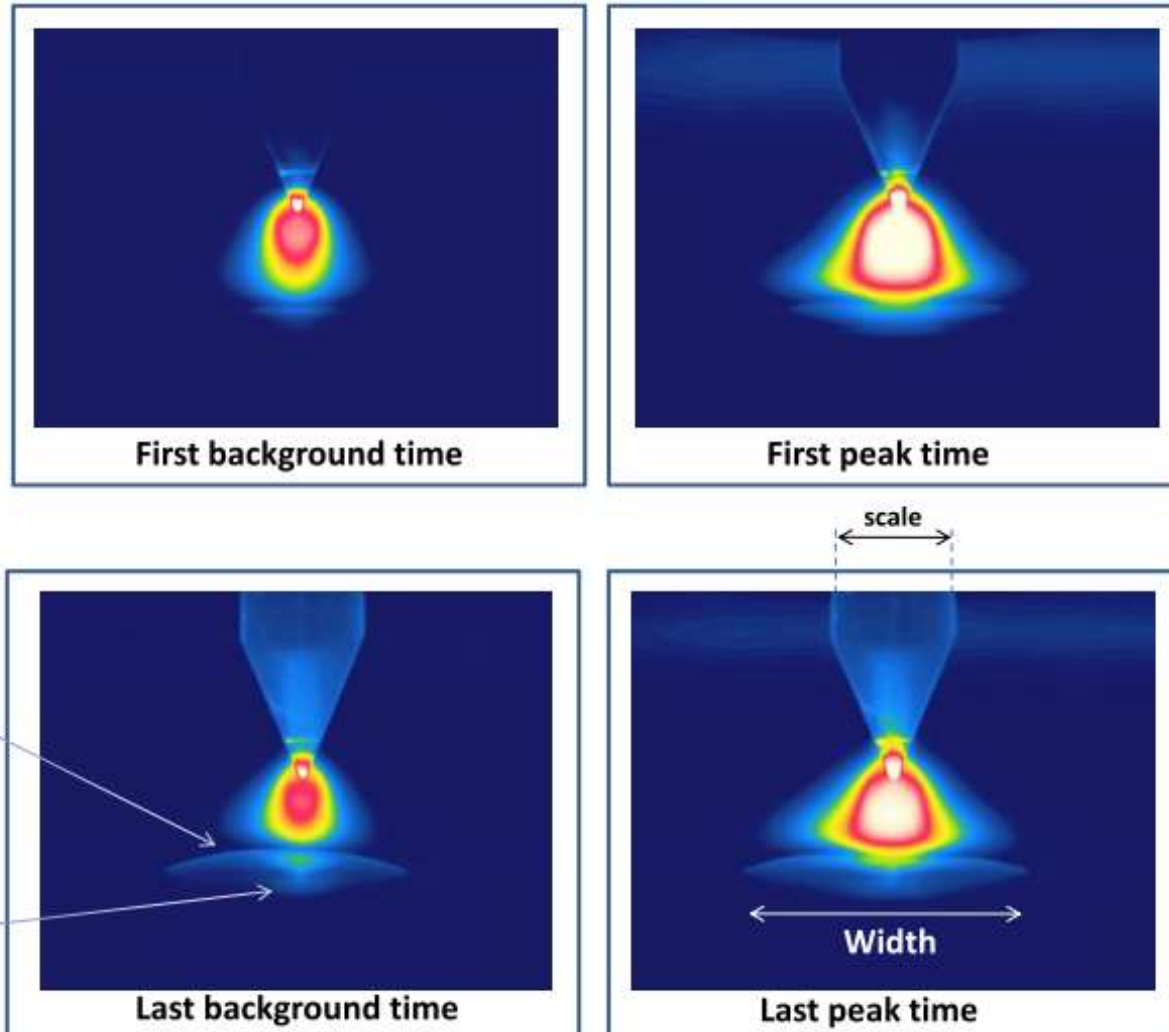
Solutions at t=4.5 s and t=5 s



Free surfaces shape at different times

► Experimental procedure

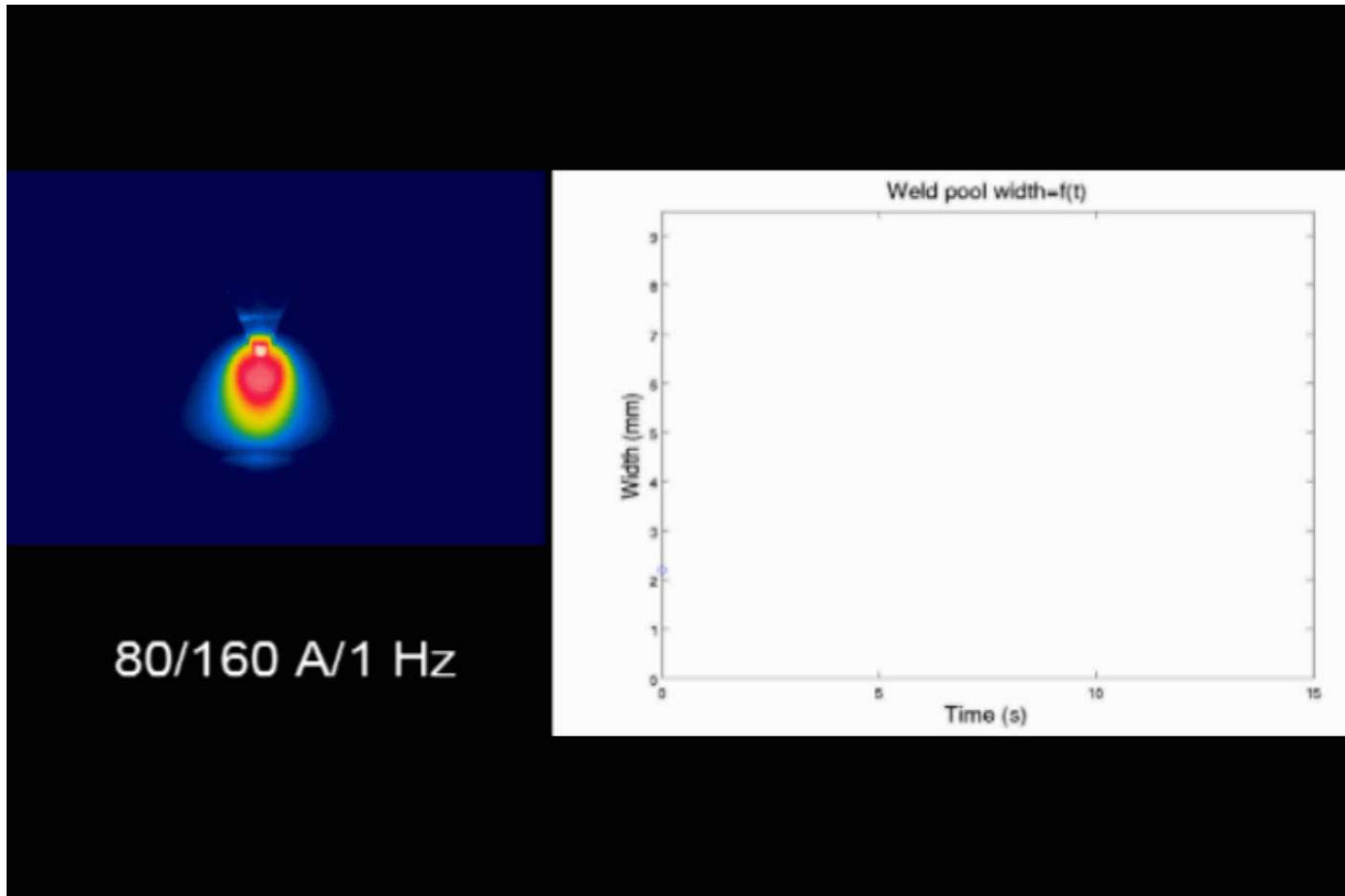
➡ *Observation of the weld pool using an IR camera*



► Validation

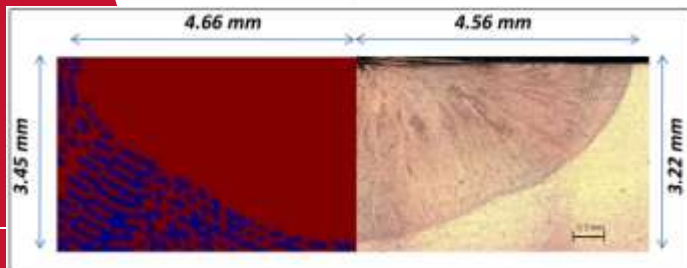
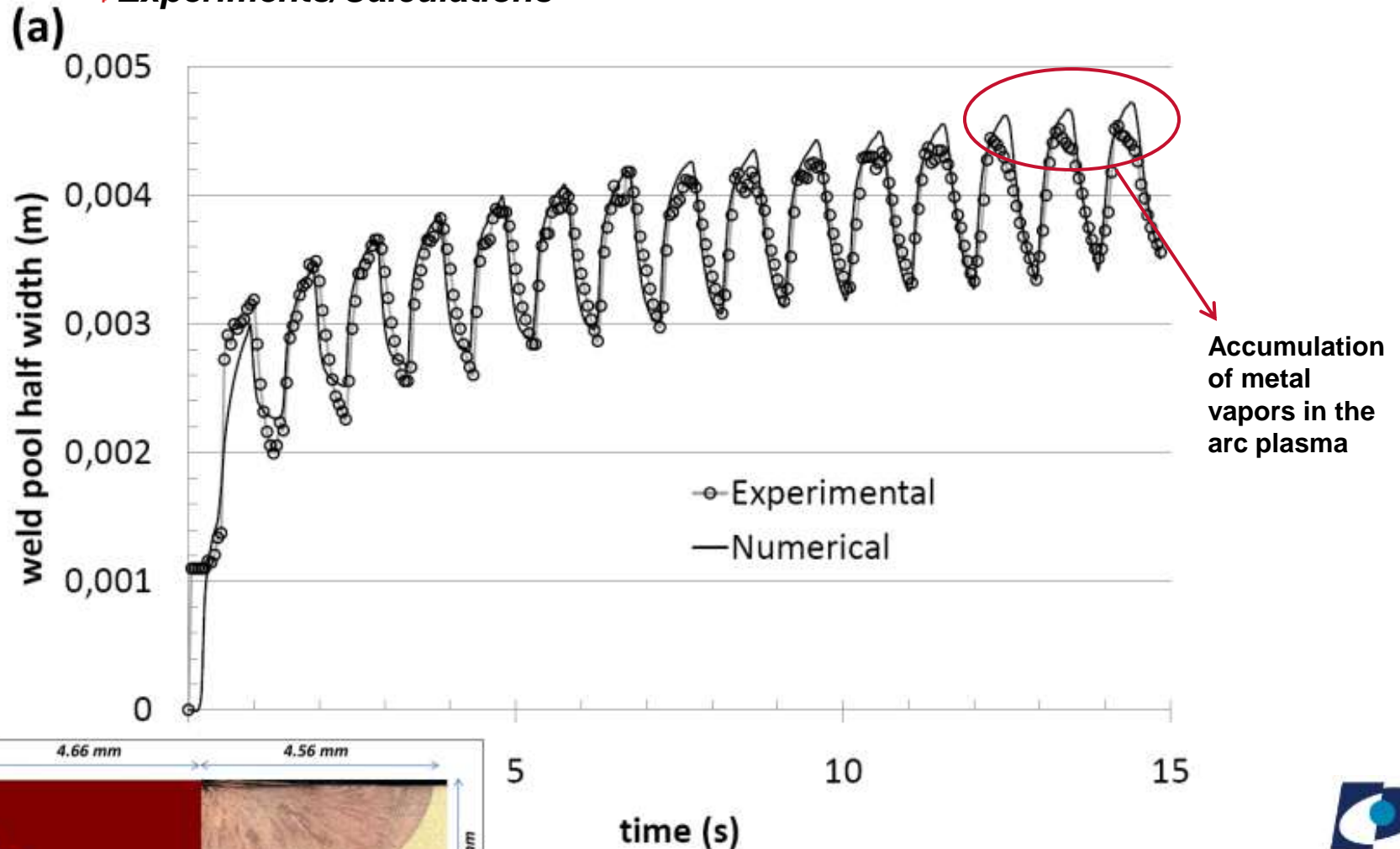
► *Experimental width of the weld pool*

Matlab image processing algorithm



► Validation

► Experiments/Calculations



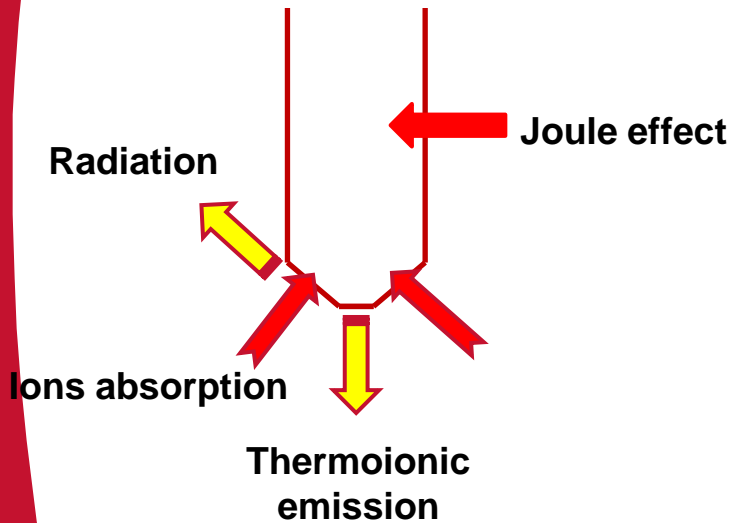
Thank you for your attention,

Any questions ?

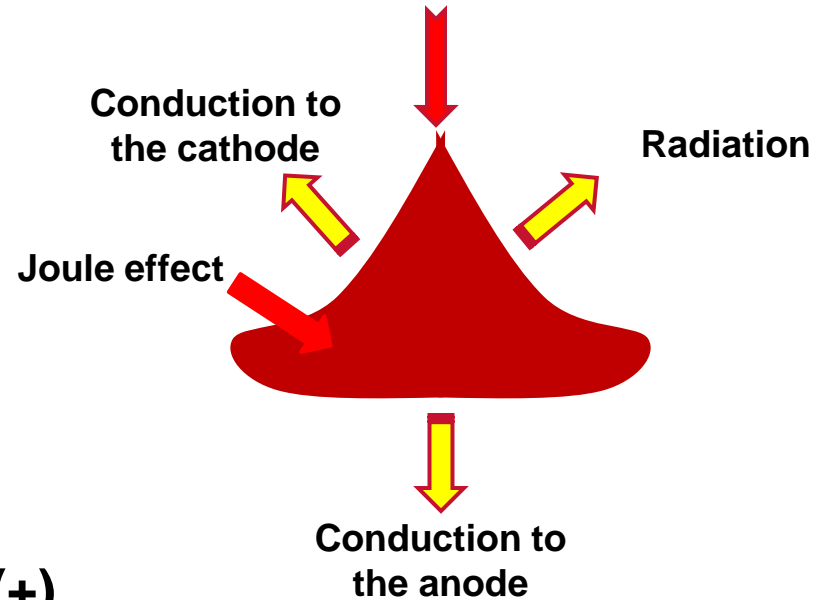
► Appendix A

Plasma physics

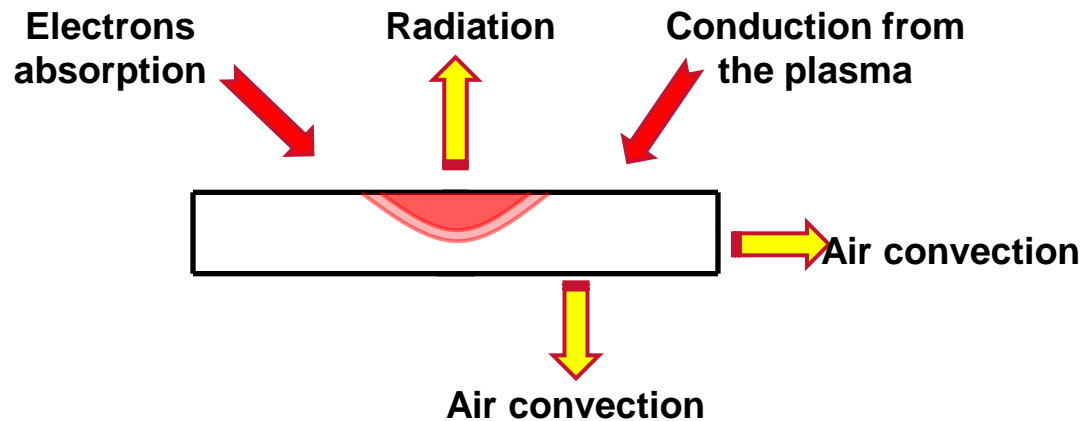
Cathode (-)



Plasma

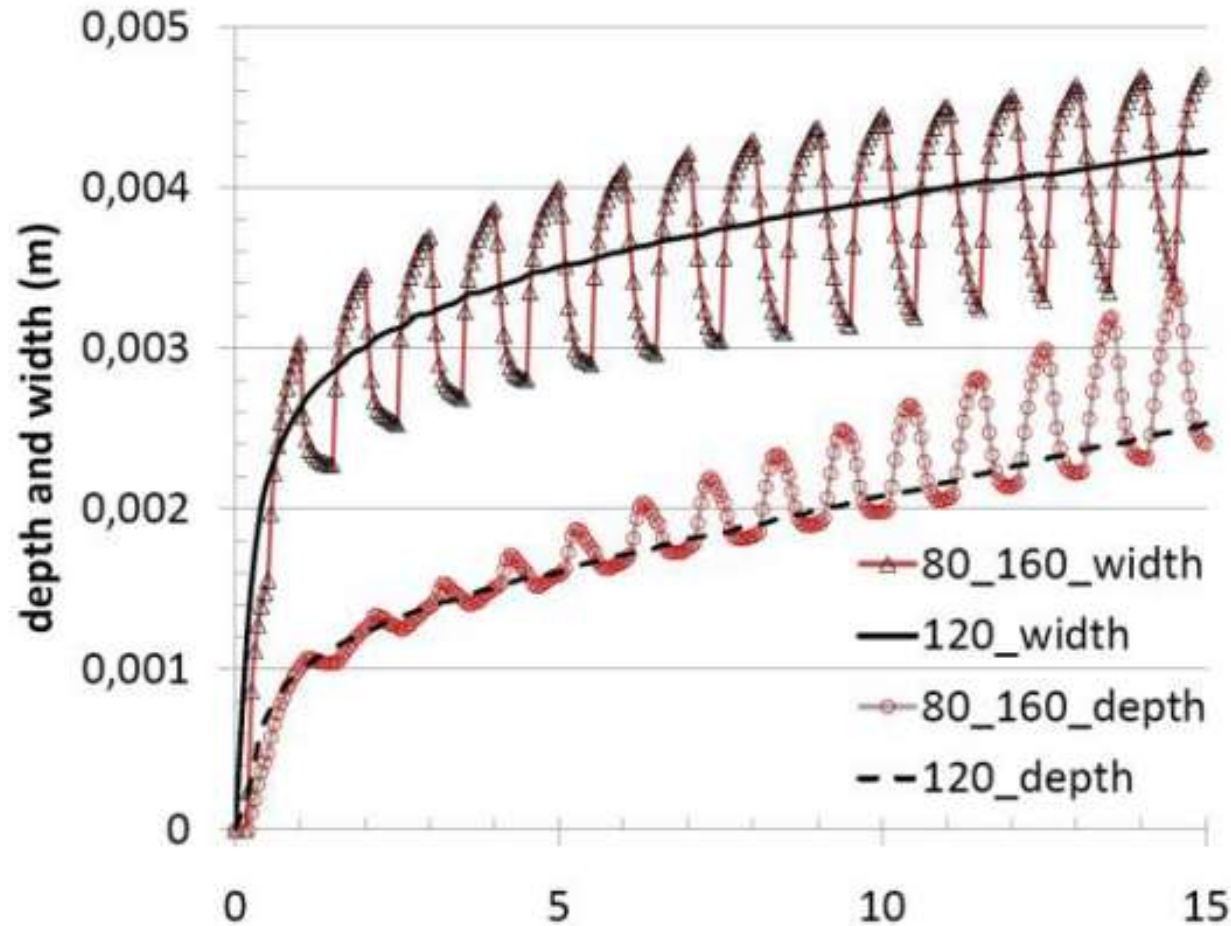


Anode (+)



► **Appendix B** *Application to pulsed current welding*

80/160 A- 1 Hz
 α 60°- h 3 mm



Weld pool dimensions for a pulsed current welding and its constant mean current